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## Vol. 89 No. 1: January (2022)



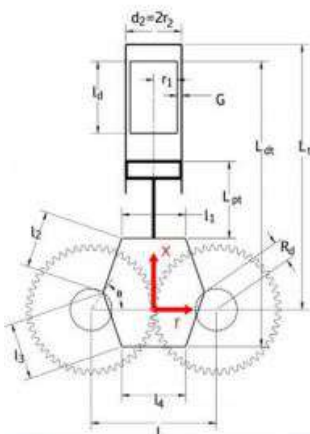
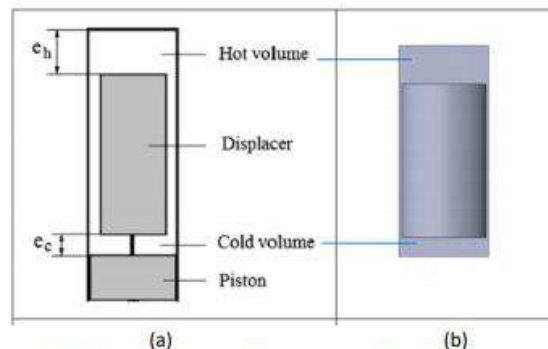
### EDITOR'S CHOICE

#### [Waste Heat Recovery of Biomass Based Industrial Boilers by Using Stirling Engine](#)

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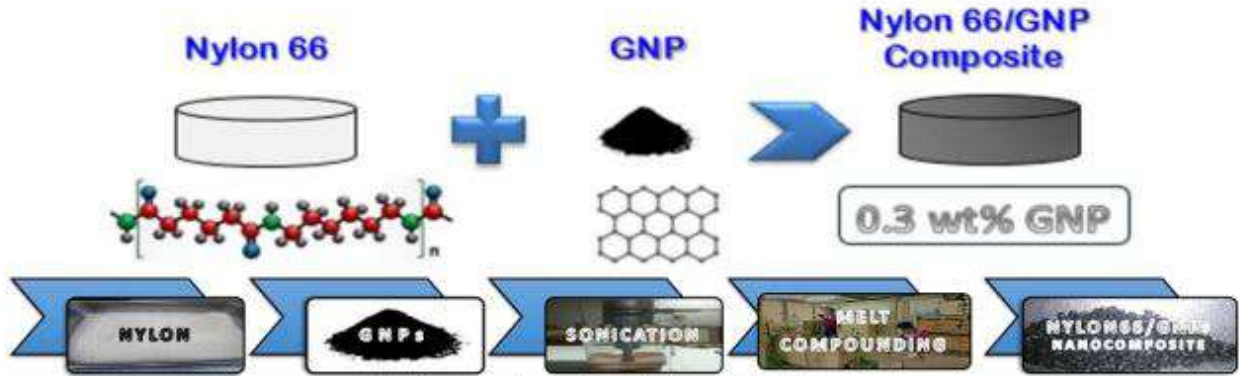


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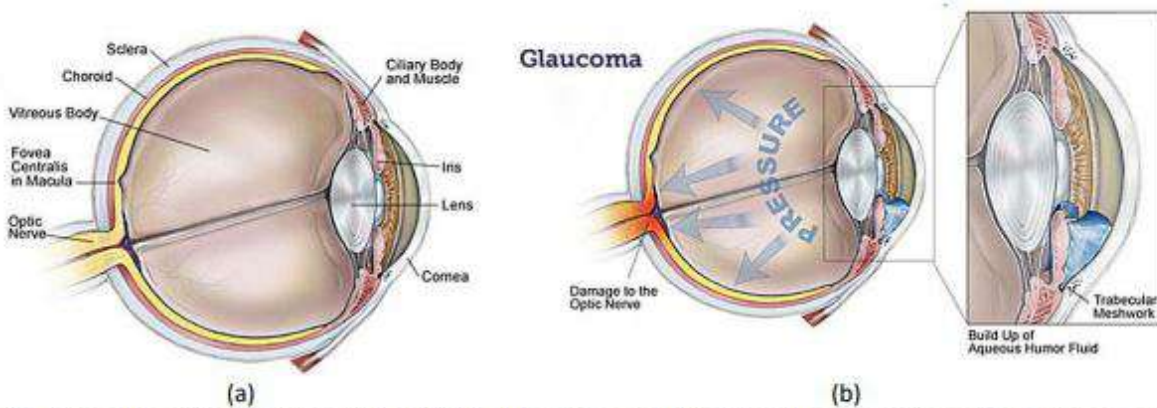


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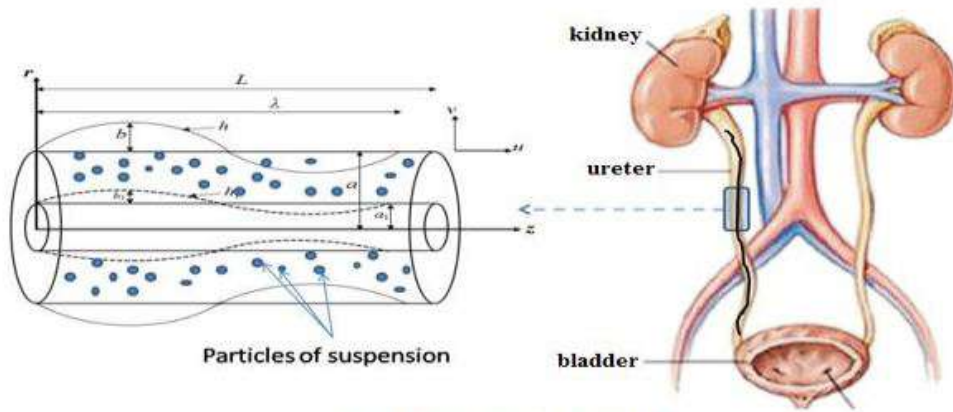


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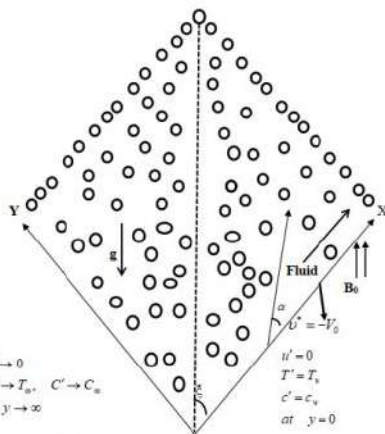


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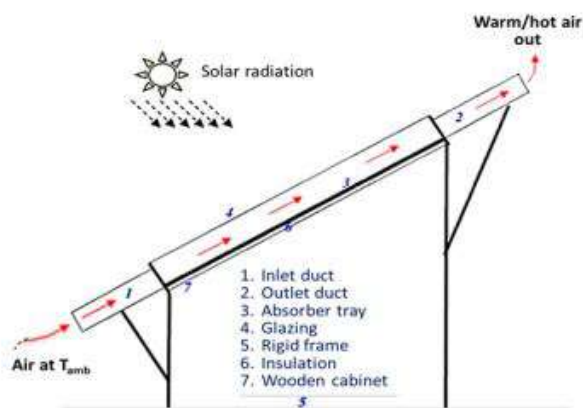


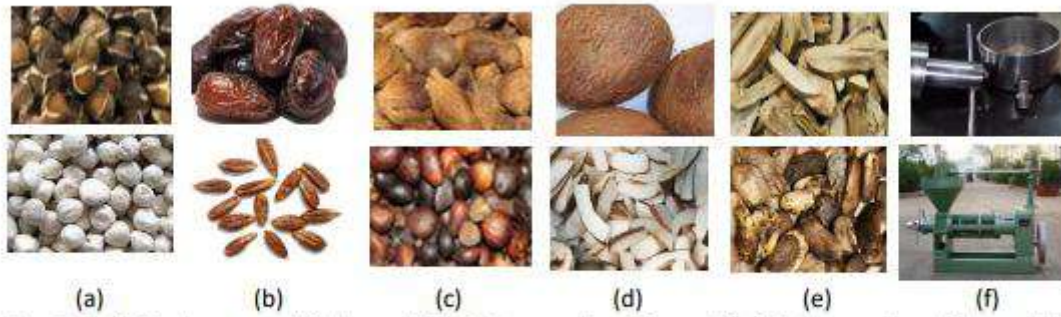
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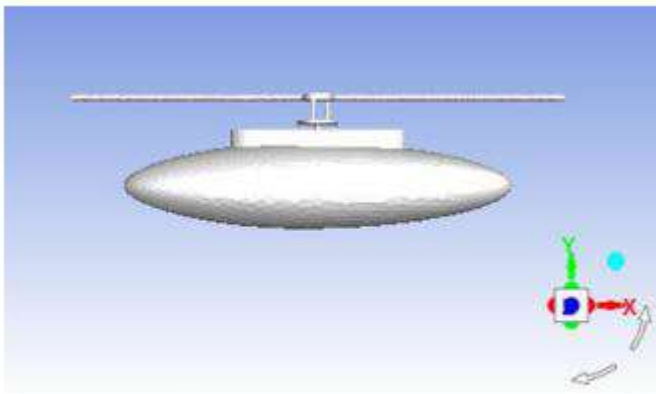
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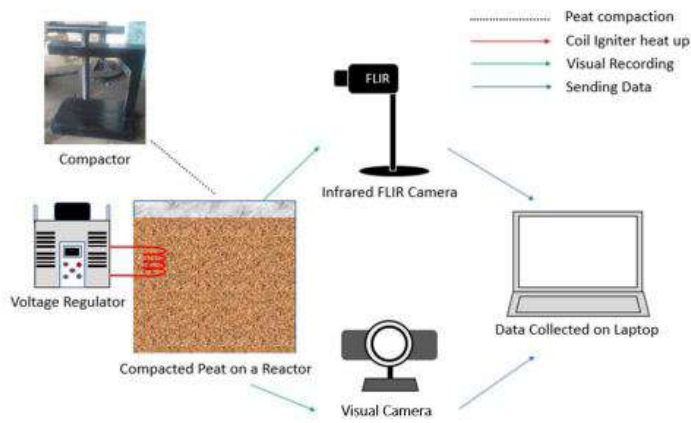


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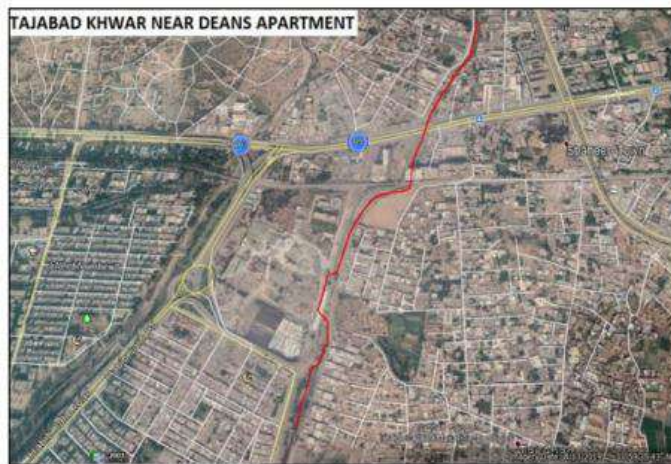


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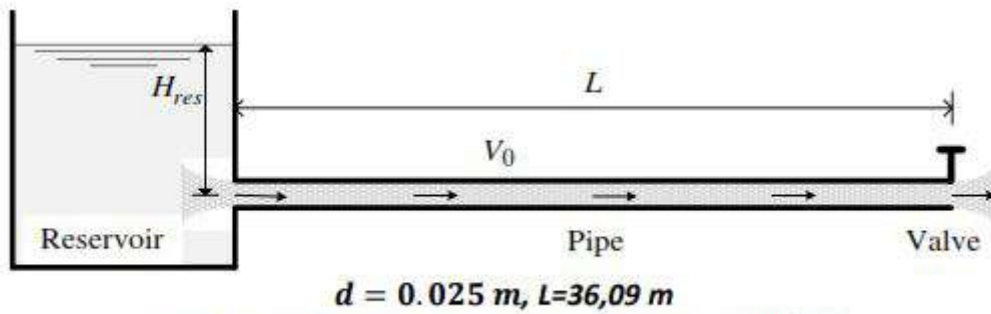


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Indonesia renewable energy potential [1]

Renewable energy form	Potential (MW)
Solar	32.654
Hydro	75.091
Wind	60.647
Bioenergy	32.654
Geothermal	29.544
Mini & Micro Hydro	19.385
Tidal	17.989
Total	443.208

## The Effect of Compression Ratio on Performance of Generator Set Fuelled with Raw Biogas

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## The Effect of Compression Ratio on Performance of Generator Set Fuelled with Raw Biogas

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### ABSTRACT

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Biogas; compression ratio; gen-set; performance; SI engine

In order to utilize a raw biogas as a fuel of generator set (gen-set), it is important to figure out optimum operating parameter of the gen-set, i.e. compression ratio. The present work aims to investigate the effect of compression ratio on performance of 3 kW gen-set fuelled with raw biogas and to obtain optimum compression ratio for operation of the gen-set on raw biogas. The gen-set used in the present work is bi-fuel engine, i.e. fuelled with gasoline or LPG. The performance of the engine fuelled with raw biogas in terms of brake power, brake torque, brake specific fuel consumption, and thermal efficiency is evaluated at compression ratio of 7.5, 8.5, 9.5, and 10.5. The work is carried out under electrical load of 240, 420, and 600 Watt. The result indicates that compression ratio affects the rotational speed, brake power, brake torque, brake specific fuel consumption, and thermal efficiency of the gen-set. Optimum compression ratio for the gen-set fuelled with raw biogas is 9.5. At the optimum compression ratio, maximum brake power, brake torque, and thermal efficiency of are 450.37 W, 1.66 Nm, and 46.93%, respectively. Minimum brake specific fuel is 0.59 kg/kWh at the optimum compression ratio.

## 1. Introduction

Many remote areas in Indonesia is still facing lack of access to electricity grid. People in those areas use either gasoline or diesel generator set to supply their electrical energy need. However, problem of fossil fuel shortage arises to them in recent years. To encounter these problems, the use of renewable energy should be adopted in electrical energy generation for rural areas. According to Indonesia Energy Projection, Indonesia has various and huge potential of renewable energy sources as can be seen in Table 1 [1]. Indonesia has renewable energy potential almost 445 MW which are in form of about 208 MW of solar energy, 95 MW of hydro power, 61 MW of wind energy, 33 MW of bioenergy, and the rest are in form of geothermal and tidal energies. However, Indonesia growth rate of renewable energy is very low, i.e. it is only 1.98% per year within the past 10 years [2]. Since bioenergy conversion system is relatively simple and low cost, biomass has a good potential to be

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converted into useful fuel, such as converted into biogas fuel via anaerobic digestion which could be applied as fuel for generator set to generate electrical energy for rural areas in Indonesia.

**Table 1**  
Indonesia renewable energy potential [1]

Renewable energy form	Potential (MW)
Solar	32.654
Hydro	75.091
Wind	60.647
Bioenergy	32.654
Geothermal	29.544
Mini & Micro Hydro	19.385
Tidal	17.989
Total	443.208

The use of alternative fuel for internal combustion (IC) engine has got more attention in recent years. Shortage of fossil fuel and its effect on global warming are the reasons behind the effort in searching an alternative fuel for IC engine worldwide. Various alternative fuels, for example biodiesel, ethanol, and biogas have been investigated as a fuel of IC engine, either compression ignition (CI) engine or spark ignition (SI) engine. Linn *et al.*, 2020 [3] applied a palm oil methyl ester biodiesel as a fuel of direct injection CI engine. A blend of ethanol-gasoline as fuel of SI engine has been widely reported by many researchers [4-10] and ethanol as fuel of CI engine has been reported by Zulkurnai *et al.*, 2020 [11]. Simulation work of CI engine also performed in order to increase thermal efficiency of the engine and reduce NO<sub>x</sub> emission [12]. Meanwhile, the use of biogas as IC engine fuel has been presented and reported by several researchers worldwide [13-16]. Review article of biogas application in IC engine also reported by Qian *et al.*, 2017 [17]. Reddy *et al.*, [15] investigated the performance and exhaust gas emission of 1.4 kVA generator set fuelled with raw biogas. The maximum power output and brake thermal efficiency were found to be 812 W and 19.50%, accordingly. Meanwhile, carbon monoxide and hydrocarbons considerably reduced whereas nitrogen oxides concentration levels did not change significantly. Due to lower calorific value of the raw biogas than LPG, they also mentioned that power of the engine deteriorated about 32% when run on raw biogas. Faria *et al.*, [13] performed zero differential thermodynamics equation simulation to predict the performance of an engine-generator unit fuelled with sewage biogas. The simulation showed that the model was successful in predicting how engine operating parameters can affect its performance and can be easily adapted to operate under different biogas compositions. In order to improve engine performance as well engine stability, Jatana *et al.*, [16] proposed strategy for high efficiency and stability of biogas engine. The work obtained that combustion was fairly sensitive to the ignition strategies which in turns affected output power and continuous fuel injection was preferred that conventional intake system especially low load engine. The proposed that a combination of technologies such as lean burn, fuel injection, and dual spark plug ignition can provide highly efficient and stable operation in a biogas-fuelled small S.I. engine, especially in the low power range of 450–1000 W. The use of injection system for biogas fuelled engine was also proposed by Iremescu *et al.*, [18]. By proper controlling of biogas injection to the combustion chamber, they found that significant improvements in fuel conversion efficiency and reductions of carbon monoxide and unburned hydrocarbons emissions.

Biogas is a gaseous fuel obtained from anaerobic digestion of various biomass feedstocks. The biogas constitutes mainly methane and carbon dioxide [19] and other gases, such as hydrogen, hydrogen sulphide, ammonia, and nitrogen. Table 2 shows a typical biogas composition [20]. However, the composition of biogas is very much depended on biomass type and properties. The



physical, chemical and biological characteristic of biomass feedstock can affect the biogas composition and yield [21].

**Table 2**  
Typical composition of biogas

Constituent	Concentration (%)
Methane (CH <sub>4</sub> )	55-60
Carbon dioxide (CO <sub>2</sub> )	35-40
Hydrogen (H <sub>2</sub> )	2-7
Hydrogen sulphide	2
Ammonia (H <sub>2</sub> S)	0 – 0.05
Nitrogen (N)	0-2

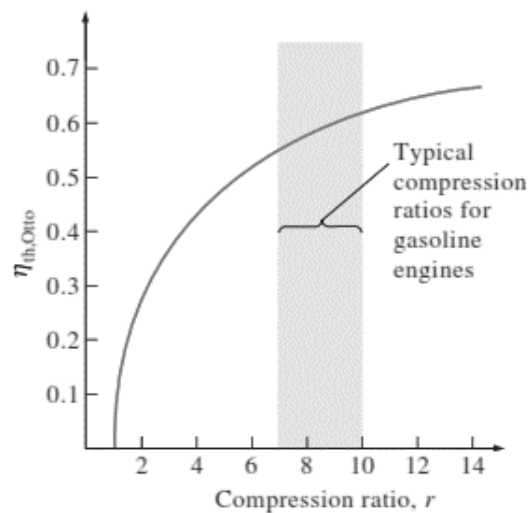
Composition of biogas plays an important role in performance of the biogas fuelled engine. Verma *et al.*, [14] evaluated performance and exhaust gas emission of compression ignition engine fuelled with various biogas composition. They employed exergy analysis in their investigation. They obtained that biogas dual fuel operation showed 80–90% diesel substitution at lower engine loads. At higher loads, total irreversibility of the engine was increased from 59.56% for diesel operation to 61.44%, 64.18% and 64.64% for BG93, BG84 and BG75 biogas compositions respectively. Moreover, combustion irreversibility was found to be decreasing with higher CO<sub>2</sub> concentrations in biogas. BG93 showed comparable results to that of diesel operation with 26.9% and 27.4% second-law efficiencies accordingly. Meanwhile, Sendzikiene *et al.*, [22] studied experimentally an impact of bio-methane gas on energy and emission characteristics of a spark ignition engine. The work found that an increase in added bio-methane gas results the drop in engine power output. Two primary effects are the cylinders were refilled less effectively and reduction in the thermal efficiency of the engine. The second effect can be partially improved by accelerating the combustible ignition mixture. They were also observed that CO<sub>2</sub> in biogas suppress combustion process which increases the content of carbon monoxide (CO) in exhaust gas, but reduces emissions of nitrous oxide (NO<sub>x</sub>). Whereas, Karagoz *et al.*, [10] investigated an effect of CO<sub>2</sub> ratio in biogas on the performance and vibration of spark ignition engine. The reported finding were the amplitude of the engine vibration increased as the CO<sub>2</sub> ratio in the biogas and the engine load increased and on contrary by decreasing the CO<sub>2</sub> ratio and increasing the engine load, cylinder pressure increased and brake specific fuel consumption decreased. They also stated that The CO<sub>2</sub> in biogas is an important compound that affects its lower heating value (LHV), burning characteristics and exhaust emissions.

In order to obtain the best performance of the engine, selection of optimum operating parameter had to be considered during application of alternative fuel for IC engine. Compression ratio, one of many operating parameters, plays an important role on performance of the engine. Theoretically, performance of the engine increases as increasing compression ratio. Brake torque of single cylinder SI engine fuel with ethanol-gasoline blend was found slightly increased as compression ratio increases from 8 to 10 without knock occurrence [23]. They also stated that CO and HC emission decreased as improving compression ratio. No significant increasing of brake torque was observed when compression ratio stepped up to 13 [24]. Increasing compression ratio resulted in increasing thermal efficiency of the SI engine fuelled with biogas [25]. They mentioned that the engine reached the maximum thermal efficiency at compression ratio between 13 and 15. The use of high compression ratio is limited by octane number of the fuel. Higher the octane number of the fuel, the higher the compression ratio can be set. Biogas has octane number of 130 [15].

In four stroke SI engine, compression ratio is defined as a ratio between maximum cylinder volume when the piston at bottom dead centre (BDC) to the minimum cylinder volume when the



piston at top dead centre (TDC). However, the selection of compression ratio is limited by octane number of the fuel. Typically, compression ratio of spark ignition engine lies between 7 and 10 as shown in Figure 1. By increasing compression ratio, thermal efficiency of the engine increases [26]. Combustion characteristic of the biogas is an important parameter that has to be considered related with compression ratio. Increasing compression ratio rises pressure as well as temperature of the mixture at the end of compression stroke. This affects the mixture burning during the combustion process of the internal combustion engine. The combustion mechanism of biogas is mainly based on the combustion of CO, CH<sub>4</sub> and H<sub>2</sub> [17].



**Fig. 1.** An effect of compression ratio on thermal efficiency [26]

### 1.1 Novelty Statement

Although an effect of compression ratio on performance of biogas engine has been reported, but the present work is different since the investigation is conducted in spark ignition engine of generator set. The present work purposes to obtain an optimum compression ratio of single cylinder SI engine of portable generator set. Performance of the engine in terms of brake power, brake thermal, brake specific fuel consumption, and thermal efficiency are investigated at compression ratio of 7.5, 8.5, 9.5, and 10.5 under variation of electrical load of 60, 240, 420, 600, 780 Watt.

## 2. Methodology

### 2.1 Experimental Setup

In the present experimental work, the effect of compression ratio of 7.5, 8.5, 9.5, and 10.5 on rotational speed, brake power, brake torque, brake specific fuel consumption, and thermal efficiency of 3 kW generator set fuelled with a raw biogas was investigated. The raw biogas is collected from biogas digester using 3 kg LPG tank. The raw material for producing a raw biogas is a cow dung. For each compression ratio, the generator set was loaded under electric load of 60, 240, 420, 600, 780 Watt. Figure 2 displays an experimental setup of the present work. The engine of the generator set is basically Bi-fuel engine where it can be fuelled with either gasoline or Liquid Petroleum Gas (LPG). Specification of the engine is given in Table 3. The electrical load panel is assembled from 15 electric bulbs, each of them has capacity of 60 Watt. Volumetric flow rate of the biogas is measured using a rotameter. Voltage and ampere of the generator are measured using a voltage and an ampere meter.

Meanwhile, engine rotation is obtained by measuring engine shaft using a tachometer. In the standard condition, the engine has compression ratio of 8.5 which its maximum and clearance volume are 196 cc and 23 cc. In order to reduce or to increase compression ratio, the cylinder head of the engine is modified. To obtain compression ratio of 7.5, the cylinder head is trimmed in such away the clearance volume becomes 26 cc. Meanwhile to set the compression ratio of 9.5, the additional packing is attached on the internal surface of cylinder head in such away the clearance volume becomes 20.6 cc

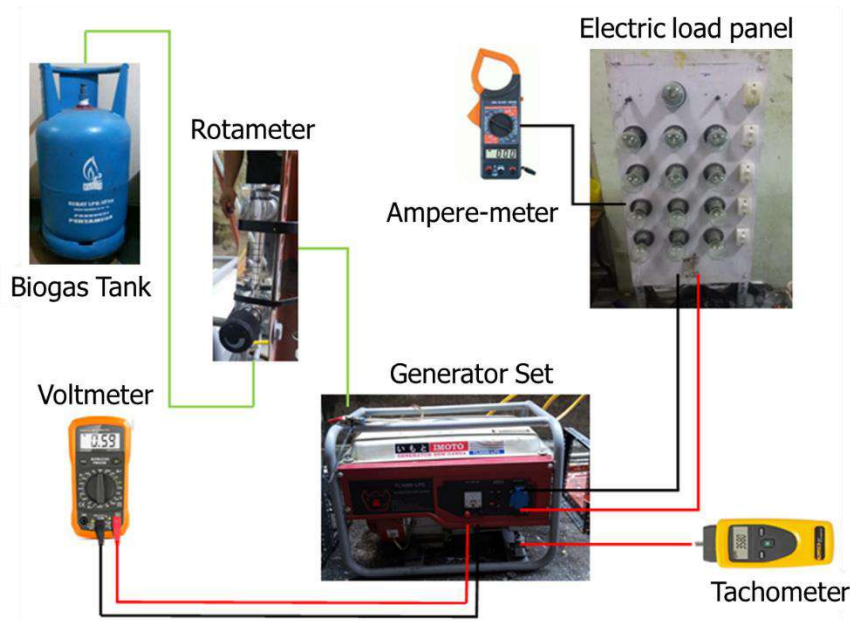


Fig. 2. Experimental setup

**Table 3**  
 Specification of the engine

Engine	Specification
Fuel	Bi-fuel (Gasoline or LPG)
Type	4-stroke, OHV, single cylinder, 196 CC
Power	3 kW at rated speed 3000 rpm
Compression ratio	8.5 (Standard)
Cooling system	Air cooled

## 2.2 Calculation of Parameters

Mass flow rate of a biogas into the engine is calculated from its volumetric flow rate read on the rotameter. Eq. (1) is used to calculate mass flow rate of a biogas

$$m_f = \frac{Q_f}{\rho_b} \quad (1)$$

where  $Q_f$  is the volumetric flow rate,  $\rho_b$  is the density of the biomass,  $1.12 \text{ kg/m}^3$  [10]. Meanwhile, brake torque ( $T$ ), brake power ( $P_b$ ), brake specific fuel consumption (bsfc), and thermal efficiency ( $\eta_{th}$ ) are calculated with Eq. (2) to Eq. (5) [15]

$$T = \frac{P_b}{2 \pi N} \quad (2)$$

$$P_b = V \times I \quad (3)$$

$$bsfc = \frac{m_f}{P_b} \quad (4)$$

$$\eta_{th} = \frac{P_b}{m_f \times LHV_f} \quad (5)$$

where N is the engine's shaft rotational speed (rpm), V and I are the voltage (Volt) and the electric current (Ampere), and LHV<sub>f</sub> is the lower heating value of the fuel (17 MJ/kg) [15]

### 3. Results

Figure 3 shows engine rotational speed at compression ratio of 7.5, 8.5 and 9.5. Engine speed decreases as electric load increases for all observed compression ratio. Theoretically, the engine rotational speed should not reduce since the generator is equipped with a mechanical governor. The governor adjusts the fuel flow rate according to the load applied on the engine. Governor regulates amount of fuel injected to the combustion chamber. More amount of fuel is injected at higher load, thus the engine speed is kept constant. However, the reduction of engine rotational speed is observed at increasing electric load during the investigation. This is due to a low pressure of biogas in the cylinder which means that the amount of biogas used is limited. The amount of biogas supplied to the combustion chamber is less than the requirement at increasing electrical load, even though the biomass flow rate is controlled by the governor.

Significant reduction in engine rotational speed occurs as increasing electric load at compression ratio of 7.5. The reduction is lower at compression ratio 8.5 and 9.5. The engine rotational speed relatively stable at compression ratio 8.5 for all electrical load observed. The pressure at the end of compression stroke steps up as increasing compression ratio and results in better combustion occurs during combustion process, and obviously generate more power to overcome the electric load of the generator. However, the engine rotational speed at compression ratio 9.5 is less stable than that at compression ratio 8.5. Compression ratio increases further up to 9.5, the pressure and temperature inside the cylinder also further increases which may cause knocking during combustion process. As we know that, the compression ratio of SI engine is limited by octane number of the fuel.

From Figure 3, it can be seen that very high engine rotational speed is observed at electric load of 60 W. This may due to sudden opening of fuel valve from the biogas cylinder to the engine, which causes more amount of biogas flows to the combustion chamber, results more power developed. Meanwhile the electric load applied is only 60 W, thus the engine rotational speed steps up abruptly from its rated speed, i.e. 3000 rpm. In order to get more comprehensive result of an effect of compression ratio on engine rotational speed, the engine has to be tested at its rated speed, such that at 3000 rpm. In accordance with generator frequency and power output ( $P = V I \cos \phi$ ), the engine rotational speed should be at 3000 rpm  $\pm$  200 rpm.

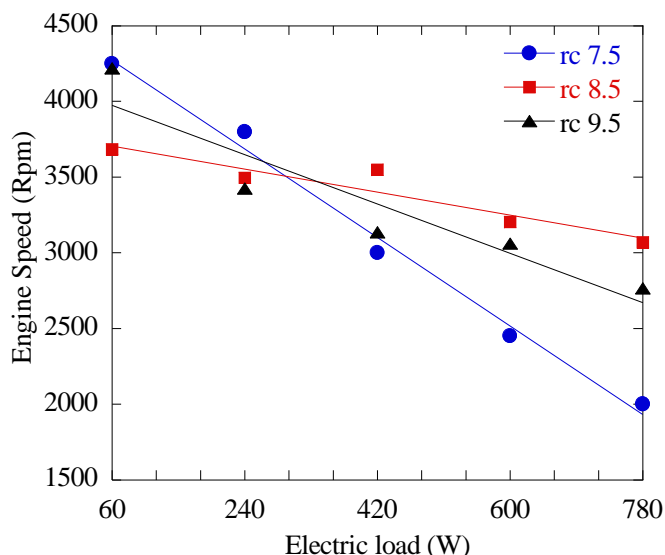


Fig. 3. Engine speed

Figure 4 and Figure 5 display brake power and torque of the engine. Similar trend between power and torque are observed. The brake power and torque of the engine incline as increasing compression ratio from 7.5 to 9.5 and decline from compression ratio 9.5 to 10.5 under all load conditions. Higher compression ratio results in higher cylinder pressure, thus higher work done on the piston during power cycle of the engine and, consequently generates higher brake power and torque. Maximum brake power and brake torque occur at compression ratio of 9.5. The maximum brake power of 450.37 W and brake torque of 1.66 Nm are observed under load test of 600 W. Further increasing compression ratio from 9.5 to 10.5, the brake power and torque decline. It may be due to abnormal combustion occurs at compression ratio of 10.5. The mixture of air and biogas burnt in absence of spark from spark plug, known as detonation. The combustion occurs is due to very high cylinder pressure. This inappropriate combustion leads to decrease output power and torque of the engine. Operated at high compression ratio, the octane number of the fuel have to be high enough to prevent the detonation. The octane number of the biogas was typically 130 [15,17]

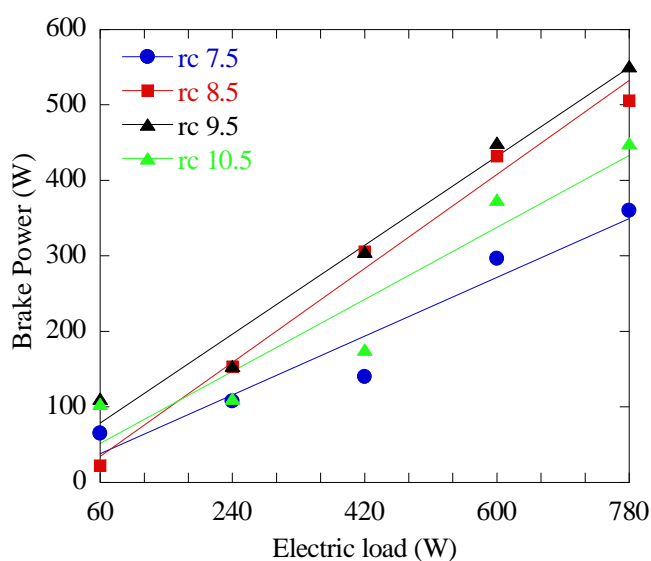


Fig. 4. Brake power

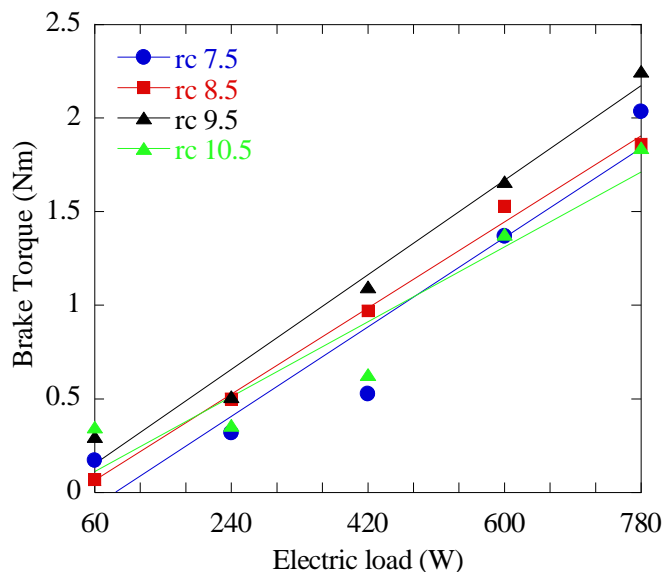


Fig. 5. Brake torque

Figure 6 presents an effect of compression ratio on brake specific fuel consumption (bsfc) of the generator set engine under load test of 240, 420, and 600 W. The bsfc declines as increasing compression ratio from 7.5 to 9.5, but it steps up when compression ratio moves to 10.5. This trend is observed for all load conditions. Typically, the bsfc ranges from 0.5 to 8 kg/kW.h in the present work. The value is comparable with the work obtained by Haryanto *et al.*, 2019 [27] whose obtained the bsfc of biogas fuel home scale genset was in the range of 2 – 17 g/W.h. The minimum bsfc at compression ratio of 9.5 is 0.59 kg/kWh under load condition of 600 W. The graph also indicates that the bsfc is lower at higher load condition. Lower the bsfc means that more efficient the engine.

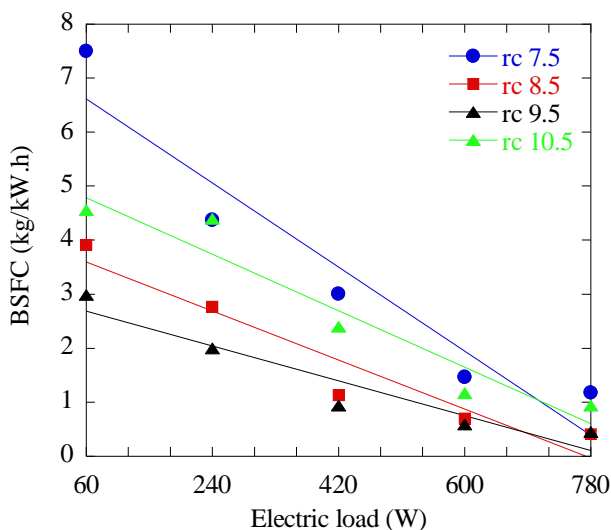


Fig. 6. Brake specific fuel consumption rate

Figure 7 displays an effect of compression ratio on brake thermal efficiency of the engine at load condition of 240, 420, and 600 Watt. Theoretically, thermal efficiency increases as increasing compression ratio. For all load conditions, the thermal efficiencies incline from compression ratio 7.5 to 9.5. However, thermal efficiency of the engine at compression ratio 10.5 is lower than the same at compression ratio 9.5. After touching maximum value at compression ratio of 9.5, the thermal efficiencies fall at compression ratio of 10.5 in the present work. Since thermal efficiency is defined

as a ratio between brake power and energy released by the fuel (Eq. (5)) in the current work, where the maximum thermal efficiency at compression ratio 9.5 is due to the highest brake power output of the engine occurs at compression ratio of 9.5. The maximum thermal efficiency of about 27% is observed at load test of 780 W.

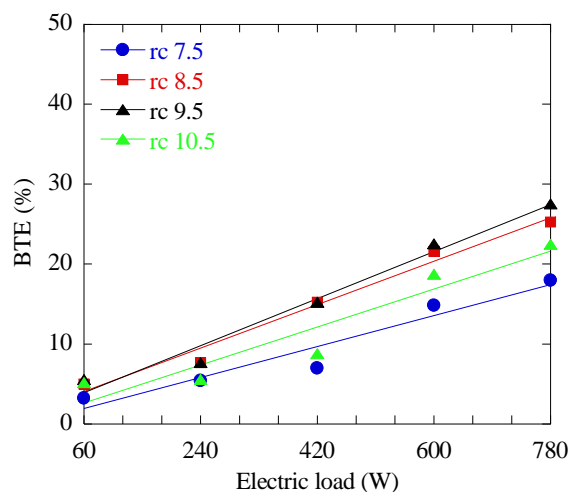


Fig. 7. Thermal efficiency

#### 4. Conclusions

Brake power, brake torque, brake specific fuel consumption, and thermal efficiency of the 3 kW generator set fuelled with raw biogas are experimentally investigated at different compression ratios. The conclusions can be drawn from the work are

- i. Compression ratio affects the brake power, brake torque, brake specific fuel consumption, and thermal efficiency of the engine
- ii. For all load condition observed, similar trend of brake power, brake torque, brake specific fuel consumption, and thermal efficiency are observed.
- iii. Optimum compression ratio for the engine fuel with raw biogas is 9.5. At the optimum compression ratio, maximum brake power, brake torque, and thermal efficiency of the engine are 450.37 W, 1.66 Nm, and 46.93%, respectively. Meanwhile, minimum brake specific fuel consumption is 0.59 kg/kWh at this optimum compression ratio.
- iv. In the future work, it is suggested that to investigate an effect of air fuel ratio and biogas pressure on performance of the engine ,

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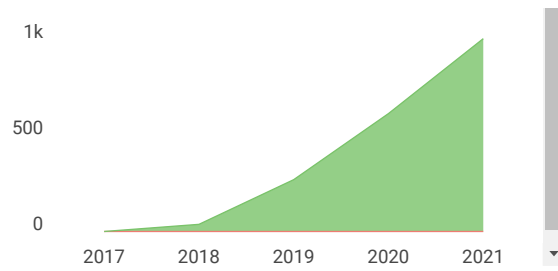
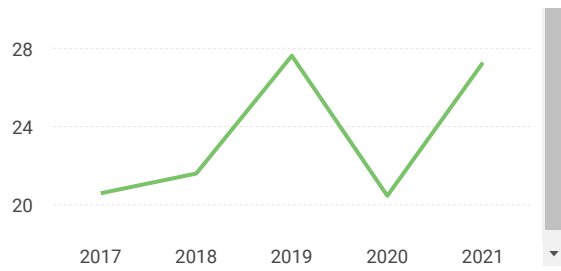
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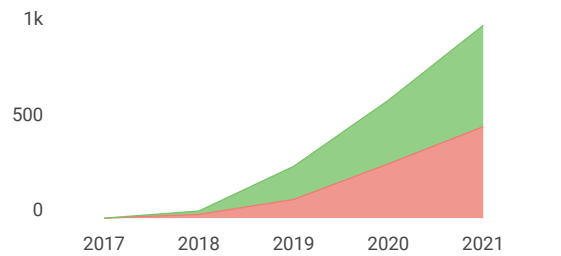
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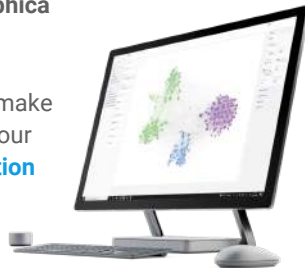
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